1	Q.	Please provide backup for the summary capital cost estimate in Table 9.1 of Exhibit
2		5d – Round Pond Hydroelectric Development Feasibility Study
3		
4		
5	Α.	The report filed as Exhibit 5d represents the level of detail that Hydro has for this
6		site. No additional detail for the summary capital cost estimate in Table 9.1 is
7		available.

1	Q.	Please provide a project description and schedule for the systems improvements
2		outlined in Section 2.4.3 of document DC1210_filed.pdf "HVDC Sensitivity
3		Studies", July 2010 required to mitigate the 3 phase fault at Bay d'Espoir. The
4		system improvements noted are a cross tripping/over frequency protection
5		system, a new 230 kV circuit between Bay d'Espoir and Western Avalon, plus two
6		new 230 kV circuits between Bay d'Espoir and Sunnyside.
7		
8		
9	A.	Stability studies of the existing Island system under peak load conditions
10		demonstrate that a 230 kV three phase fault at Bay d'Espoir with tripping of a
11		230 kV transmission line between Bay d'Espoir and Sunnyside will result in
12		angular instability. In other words, the system does not recover from the fault
13		and an outage will occur. To the extent that the existing AC system cannot
14		survive a three phase fault at Bay d'Espoir during peak load conditions, the
15		DC1210 – "HVDC Sensitivity Studies" contemplated an Island system with an
16		HVdc interconnection having performance similar to the existing Isolated Island
17		Scenario. This was outlined in section 2 of the study, last paragraph of page 2-1
18		which states:
19		
20		It is also based on the assumption that the three-phase
21		Bay d'Espoir fault will not be considered when determining
22		the synchronous condenser requirements and system
23		upgrades. This fault is not considered in this sensitivity
24		analysis as the intent is to determine the system additions
25		for the HVdc integration with system performance
26		comparable to that of the existing system.
27		

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1	For clarification, Section 2.4.3 of DC1210 – "HVDC Sensitivity Studies" does not
2	state that two new 230 kV circuits between Bay d'Espoir and Sunnyside are
3	required to mitigate a 3 phase fault at Bay d'Espoir.
4	
5	Section 2.4.3 states at page 2-5:
6	However, if the new 230 kV circuit between Bay d'Espoir
7	and Western Avalon is built and if this new circuit plus the
8	two circuits between Bay d'Espoir and Sunnyside are 50%
9	series compensated, AND if 2x300 MVAR high inertia
10	Toshiba synchronous condensers are in service at Soldiers
11	Pond (which means 3x300 MVAR installed to account for
12	maintenance outages), the system is able to recover from
13	a three-phase fault at Bay d'Espoir within criteria.
14 15	The "two circuits between Bay d'Espoir and Sunnyside" refer to the two existing
16	circuits between these locations (i.e. TL202 and TL206).
17	
18	The upgrades necessary to recover from a three phase fault at Bay d'Espoir are:
19	
20	1) A new 230 kV circuit between Bay d'Espoir and Western Avalon
21	This circuit is common to both the Interconnected and Isolated scenarios, and is
22	included in NL Hydro's 2012 capital budget submission. Construction of the 230
23	kV transmission line between Bay d'Espoir and Western Avalon has a five year
24	completion schedule and includes:
25	• Addition of three 230 kV circuit breaker bays at Bay d'Espoir Terminal
26	Station #2 to complete the breaker and one half arrangement on legs 1
27	and 2 with the new line termination on leg 3;

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1	Construction of 188 km of overhead 230 kV transmission line consisting
2	of 795 kcmil ACSR "DRAKE" conductor on steel towers with overhead
3	shield wire along the entire length; and
4	• Addition of a four 230 kV GIS circuit breaker ring bus arrangement at
5	Western Avalon.
6	
7	2) Three 300 MVAR high inertia synchronous condensers at Soldier's Pond.
8	Three 300 MVAR units are currently in the Basis of Design for the Labrador-
9	Island Transmission Link, but quantities and final rating will be determined
10	during detailed engineering. The applicable design criteria will be to ensure
11	that the Island system remains stable for faults under which the Island
12	system remains stable today.
13	
14	3) 50% series compensation of the two existing and one new transmission line
15	(from (1)) between Bay d'Espoir and Sunnyside. This work is neither
16	budgeted nor scheduled. Nalcor has not opted to install the series
17	compensation on each of the three 230 kV transmission lines between Bay
18	d'Espoir and the eastern portion of the system. Given the extremely low
19	probability of the event, the increase in cost for series compensation in the
20	HVdc scenario was deemed to unnecessarily penalize the Interconnected
21	Scenario over the Continued Isolated Scenario from a performance
22	perspective.
23	
24	Similar to the existing Island System, there are load scenarios in the
25	interconnected case where the system will survive the 230 kV bus fault at Bay
26	d'Espoir. Preliminary analysis of the Interconnected System with a simplified
27	model of the Labrador – Island HVdc Link reveals that the Island System will

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1	remain stable following a three phase fault at Bay d'Espoir with the 230 kV
2	transmission line between Bay d'Espoir and Western Avalon added and all
3	synchronous condensers in service during the spring/fall intermediate load
4	levels.

5

1	Q.	Please provide project scoping documents, cost estimates, and relevant technical
2		details of these system reinforcements referred to in MHI-NALCOR-86.
3		
4		
5	Α.	No additional system reinforcements are planned to mitigate a 3 phase fault at Bay
6		d'Espoir. As a result, no documents exist.

1	Q.	Are there any load/generation patterns on the Island where the system survives a 3
2		phase fault at Bay d'Espoir, and will implementing the system reinforcements listed
3		in DC 1220, section 2.4.3 change this result?
4		
5		
6	Α.	DC 1210 section 2.4.3 provides the system reinforcements for the Island system
7		specific to an interconnected Island scenario including an HVdc transmission line
8		between Labrador and the Island portion of the province as discussed in MHI-
9		Nalcor-83. There are two loading scenarios where the isolated Island system
10		maintains angular stability today for a 230 kV three phase fault at Bay d'Espoir with
11		subsequent tripping of a 230 kV transmission line between Bay d'Espoir and
12		Sunnyside. These loading scenarios are:
13		
14		Intermediate system load levels where in service Holyrood generators are
15		operating at 80 MW or less; and
16		• Summer loading conditions where there are no units in service at Holyrood.
17		
18		Simulations of the isolated Island system with the proposed 230 kV transmission
19		line addition between Bay d'Espoir and Western Avalon reveal that angular stability
20		is maintained for a 230 kV three phase fault at Bay d'Espoir with subsequent
21		tripping of a 230 kV transmission line between Bay d'Espoir and Sunnyside.
22		
23		For the continued isolated Island system, the most severe ac system fault is a 230
24		kV three phase fault at Holyrood. A 230 kV three phase fault at Holyrood will result
25		in severe voltage dips to plant auxiliaries resulting in tripping of all on line
26		generators and subsequent loss of angular stability. The system reinforcements

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- 1 proposed under DC 1210 "HVdc Sensitivity Studies" will not improve the angular
- 2 stability of the isolated system for a 230 kV three phase fault at Holyrood.

1	Q.	Are any further system reinforcements planned or required to mitigate a 3 phase
2		fault at Bay d'Espoir?
3		
4		
5	Α.	No further system reinforcements are planned to mitigate a three phase fault at
6		Bay d'Espoir.

1	Q.	The assumption of annual capacity factor of 40% for the 25 MW wind farm is based
2		on the average of the two existing wind farms at St. Lawrence (44.3%), and Fermeuse
3		(35.7%) capacity factors. Has any wind survey data been collected to validate the
4		assumption of a 40% capacity factor at the proposed site of the 2014 3rd 25 MW
5		wind farm? If so, please provide documentation to support the anticipated capacity
6		factor.
7		
8		
9	A.	It is assumed that the site of the proposed 2014 3^{rd} 25 MW wind farm would be
10		chosen through an RFP process.
11		
12		Submissions from proponents other than St. Lawrence and Fermeuse through
13		Hydro's 2005 and 2006 Wind RFP process indicated expected net annual capacity
14		factors ranging from 35% to 43%. Accordingly, the use of an average of the capacity
15		factors of the two existing wind farms (or the approximate midpoint of the range of
16		capacity factors submitted in the RFP) is reasonable in comparison with the range of
17		other prospective sites on the Island.

1	Q.	Has a system study been performed that examines wind integration into the
2		Newfoundland Island power system? If so, please provide this document.
3		
4		
5	Α.	A system study has been completed to examine wind integration into the
6		Newfoundland Island power system. Please see Exhibit-61.

Q. 1 What is the maximum wind capacity sustainable on the Island under both options 2 (Muskrat Falls LIL HVDC and the Isolated Island)? 3 4 The 2004 NL Hydro study "An Assessment of Limitations For Non- Dispatchable 5 Α. 6 Generation On the Newfoundland Island System " (Exhibit 61) established two 7 limits regarding the possible level of wind generation integration on the Isolated 8 Island system, an economic limit and a maximum technical limit. The study 9 determined that for wind generation in excess of 80 MW there would be a 10 significant increase in the risk of spill at the hydroelectric reservoirs particularly 11 during the spring run off diminishing the economic advantage of additional wind 12 generation. The study further determined that for wind generation above 130 MW 13 it would not always be possible to maintain system stability particularly during 14 periods of light load and during these periods wind generation would have to be 15 curtailed. 16 17 The limits identified in the 2004 study are still applicable today. However, as load grows, the Isolated Island system should be able to accommodate additional wind 18 19 generation. It has been suggested that the system should be able to accommodate 20 an additional 100 MW of wind in the 2025 timeframe and a further 100 MW around 21 2035. Nalcor has not studied this in detail but will undertake studies prior to DG3. 22 Nalcor has not completed an analysis to establish the level of wind generation that 23 24 could be sustained in the Muskrat Falls LIL HVDC option. However, given that this 25 option will include at least one interconnection to the North American electrical 26 grid and that there will be considerable hydroelectric capacity both in Labrador and 27 on the Island to provide backup it would not be unreasonable to consider an

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1	additional 400 MW of wind generation on the Island. Nalcor will be analysing this as
2	part of the analysis that will be completed prior to DG3.
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4	
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12	

1	Q.	Please provide all historical sales, generation and peak demand information for the
2		period 1969-2010 for all sectors that are part of the Load Forecast. This would
3		include the number of customers and energy (GW.h) for the following sectors: rural
4		residential, NP residential, total residential, rural GS, small GS, large GS, electric heat
5		GS, total GS, street & area lighting, industrial and total island sales.
6		
7		
8	Α.	Please see Exhibit -58. Peak demand information is provided in the response to
9		MHI-Nalcor-92.